Enabling Ideal Selective Solar Absorption with 2D Metallic Dielectric Photonic Crystals

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The selective absorption of sunlight plays a critical role in solar-thermophotovoltaic (STPV) energy conversion by tailoring both the absorption and emission spectra for efficient solar-thermal-electrical energy conversion. By selectively absorbing solar energy while suppressing long wavelength emission, optimal solar-thermal energy conversion can be achieved. In practical STPV systems, selective absorbers must simultaneously contain optical, manufacturing, and reliability properties. Previous efforts have typically focused only on a subset of these requirements. In this communication, we present our solution which contains all of the ideal properties of a selective absorber for large-scale and efficient solar energy conversion.

The effective absorption of solar energy requires selective absorption across the solar spectrum, high temperature reliability, omnidirectional absorption, and wafer-scale fabrication for mass scalability. Recent developments of metal based selective absorbers have demonstrated 1D, 2D, and 3D metallic photonic crystal structures capable of tailoring the absorption spectrum. One dimensional metal dielectric stacks have demonstrated promising solar absorbing properties but are unstable at temperatures greater than approximately 600 °C. In particular, two-dimensional metallic air photonic crystals (MAPhC) have been shown to selectively absorb light in the near-IR via cavity modes and withstand high temperatures greater than 1000 °C; however, the acceptance angle is limited to ±30°, and the absorption in the visible spectrum is limited due to diffraction. Metamaterial and plasmonic based absorbers have demonstrated wide angle absorption due to their subwavelength periodic structures; however high temperature stability and wafer-scale fabrication have yet to be shown.

Here we present our 2D metallic dielectric photonic crystal (MDPhC) structure, which simultaneously demonstrates broadband (visible to near-IR) absorption, omnidirectional absorption, wafer-scale fabrication, and high temperature robustness. The wafer-scale fabricated MDPhC has a measured absorption of 85% for photon energies $5\text{ eV} \geq h\omega > 0.7\text{ eV}$ and an absorption below 10% for $h\omega < 0.4\text{ eV}$. Angled measurements show existence of the cavity modes for angles up to 70° from normal. Furnace tests at 1000 °C for 24 hours show a robust optical performance due to its fully encapsulated design which helps to retain the metal cavity shapes at high temperatures. Finite-difference time-domain (FDTD) and rigorous coupled wave analysis (RCWA) based simulations indicate that the broadband absorption is due to a high density of hybrid cavity and surface plasmon polariton (SPP) modes overlapped with an anti-reflection coating (ARC).

A schematic image of the MDPhC is shown in Figure 1(a) and (b). The MDPhC utilizes cut-off frequencies of cavity modes to tailor the absorption. Since the cut-off frequency is dependent on the geometry of the cavities, the absorption spectrum can be tuned by simply modifying the radius and depth of the cavities. Photos and SEM images of the device are shown in Figure 1(c)-(f) where the multilayered structure was fabricated using the sidewall lithography technique across a 6" wafer (see Supporting Information). An 80 nm thick layer of ruthenium is used as the metal, which was deposited via atomic layer deposition (ALD) for conformal deposition purposes. The dielectric filling of HfO$_2$ is also deposited via ALD, and excess HfO$_2$ is removed via chemical mechanical polishing (CMP). A layer of HfO$_2$ with a thickness of approximately $t = 25\text{ nm}$ is left on top of the entire structure. HfO$_2$ is chosen due to its conformal deposition, high melting temperature, and transparency in the visible and infrared (IR) regime. The fully fabricated 6" wafer is shown in Figure 1(c), where it has been diced into 1 cm $\times$ 1 cm chips. An angled scanning electron microscope (SEM) image of the 70 nm thick Al$_2$O$_3$ shells before the metal is deposited is shown in Figure 1(d) and of the wafer after the CMP process in Figure 1(e). A cross section SEM image obtained via focused ion beam (FIB) milling is shown in Figure 1(f) which confirms the complete filling of the metallic cavities. Due to the large area nature of the fabrication, small variations of the material thicknesses are observed which explains the reason why Figure 1(e) and (f) are slightly different, however these small variations do not significantly impact the absorption spectrum (see Supporting Information). Along with the cut-off frequency, the design of the cavities is also based on Q-matching formalism where maximum absorption occurs when the radiative $Q_{\text{rad}}$ and the absorption $Q_{\text{abs}}$ are equal.

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The measured absorption spectrum shown in Figure 2(a), demonstrates the broadband absorption of the MDPhC across the majority of the solar spectrum along with a steep cut-off frequency. A UV-Vis-near-IR Cary 500i spherical diffuse reflectance measurement accessory was used to obtain the total absolute absorption spectrum ($\alpha_t = 1 - R_t - T_t$) of the MDPhC, MAPhC, and flat ruthenium at an incidence of 3° with unpolarized light. The terms $R_t$ and $T_t$ are the total reflection and transmission values. For absorption measurements at photon energies in the IR, a Fourier transform infrared (FTIR) spectrometer was used with a commercial aluminium coated reference mirror. The FDTD simulated absorption of the MDPhC layer agrees well with experiment, but diverges for $3eV/\hbar\omega >$, where transmission through the metal layer can no longer be assumed to be constant.

Figure 1. MDPhC images. (a) Schematic diagram of the MDPhC. (b) Schematic of the cross-section of the MDPhC with period $a$, radius $r$, depths $d_1, d_2$, metal thickness $m_t$, Al$_2$O$_3$ thickness $s_t$, and ARC thickness $t$. The HfO$_2$ filling has been made transparent for clarity. (c) Photo of the fully fabricated 6° wafer. (d) SEM image of the 40 nm thick Al$_2$O$_3$ shells before metallization. (e) SEM image of the fully fabricated wafer surface. (f) SEM image of the cross-section of the MDPhC taken at a 42° angle. Measured dimensions are $a = 790$ nm, $r = 200$ nm, $d_1 = 380$ nm, $d_2 = 200$ nm, $m_t = 80$ nm, $s_t = 40$ nm, and $t$ is measured to be approximately $t = 25$ nm.

Figure 2. Absorption spectra. The total measured and simulated absorption spectrum for the (a) MDPhC and (b) MAPhC. An absorption measurement for flat ruthenium and the AM1.5 solar spectrum are shown for reference. The first three modes of the simulated spectrum are labeled as M$_1$, M$_2$, and M$_3$ for reference. The FDTD simulated absorption and transmission spectra used structures with dimensions of $a = 780$ nm, $r = 200$ nm, $d_1 = 380$ nm, $d_2 = 200$ nm, $m_t = 80$ nm, $s_t = 40$ nm and $t = 25$ nm. (c) $E_z$ field image of the M$_3$ mode. SPP modes can be seen propagating along the vertical sidewalls of the cavity at the HfO$_2$/Ru interface. (d) Simulated absorption spectrum comparing MDPhCs with and without ARC coating. Simulations of the M$_3$ mode intensity $|E|^2$ plot are shown (e) with and (f) without the ARC layer. The intensity plot with an ARC layer has a reduced reflection intensity at the top metal surface indicated by the white arrows due to destructive interference.
At these frequencies, the silicon substrate absorbs the transmitted light. The cut-off frequency is located at mode M1 with $\hbar \omega = 0.75$ eV, below which the absorption is suppressed to below 10% for $\hbar \omega < 0.4$ eV.

In comparison, the MAPhC measured absorption spectrum is shown in Figure 2(b), which has a poorer absorption profile over the visible frequencies due to diffraction losses. The MAPhC has the same dimensions as the MDPHc, however the MAPhC does not have the HfO2 filling. The cut-off frequency for the MAPhC shifted by a factor of 2.07 to 1.55 eV, which closely matches the measured index of the HfO2 in the cavity. The FDTD simulated MAPhC absorption is also shown which agrees well in frequency, but has higher absorption values than measured. Mismatch between the simulation and experiment may also be attributed to both the smooth cylindrical structure and perfect uniform geometry in the simulation that are not present in the actual device due to the large scale fabrication variation.

The broadband optical properties of the MDPHc in the visible regime are due to the combination of a high density of cavity modes and an ARC layer. The dielectric filling essentially red-shifts the frequencies of the high order cavity modes to create a high density of states in the visible regime. Experimentally, this can be observed in the larger number of peaks in the measured MDPHc absorption spectrum in comparison to the MAPhC absorption spectrum in Figure 2(a) and (b), respectively. The first two modes, M1 and M2, are standard cavity modes, however, the third mode, M3 ($\hbar \omega = 2.21$ eV) supports a hybrid cavity and SPP mode as can be seen in the E field image in Figure 2(c). The coupling between cavity and SPP modes may also contribute to the increased absorption in the M3 mode.

The wavelength of mode M3 ($\lambda_3 = 560$ nm) occurs at wavelengths below the period of the MDPHc ($a = 780$ nm) where diffraction losses typically occur. Thus, an ARC layer serves to minimize reflections at the top surface of the MDPHc and increase the absorption in the visible spectrum. To demonstrate this, Figure 2(d) shows absorption spectra of the MDPHc with and without an ARC layer; the spectrum with an ARC layer shows considerably higher absorption at the M3 mode than without an ARC layer. Figure 2(e) shows the intensity plots of the M1 mode with a reduced reflected intensity at the top metal surface due to destructive interference caused by the ARC layer in comparison to the same mode without an ARC layer shown in Figure 2(f). Furthermore, integration of the FDTD simulated Poynting vector reveals that the ARC layer causes 44% of the incident light power to be absorbed at the top metal surface for mode M3, whereas without an ARC layer only 33% is absorbed.

Analytically, the ARC layer on a flat HfO2 and ruthenium interface can be calculated by inserting the complex permittivity of the metal ($\varepsilon_{Ru}$) layer into the Fresnel reflection equation (see Supporting Information). To suppress undesired reflection in the visible spectrum of $\hbar \omega = 1.55$ eV → 3.1 eV, with an average index of HfO2 at in the visible regime of $n = 2.09$, we calculate an ARC layer thickness of $t_{ARC} = 22$ nm → 72 nm for a flat surface. Thus, if the proper ARC layer thickness is designed to spectrally overlap with the high density of optical states, high, broadband absorption will occur.

To verify the wide angle absorption properties and high temperature stability of the MDPHc, the measured spectra at various angles are shown in Figure 3. As previously explained, the dielectric filling in the MDPHc down-shifts the frequency of the low order modes to be below the diffraction threshold thus improving the wide angle absorption. Clearly, the cavity modes in Figure 3(a) remain relatively fixed in frequency as a function of angle, which is a characteristic of the cavity modes. RCWA simulations of the MDPHc absorption at incident angles up to 90° are shown in Figure 3(b) and agree well with the experimentally measured absorption spectrum in Figure 3(a). An incident planewave with both S and P polarizations
polarizations is used. The simulated average absorption for wavelengths from 2.76 eV to 0.69 eV and incident angle from 0° to 70° is 0.72. Angular dependence of the higher order absorption modes is due to diffraction effects via Wood’s anomaly and ARC angle dependence.\[30\]

The same MDPhC sample measured in Figure 3(a) was then placed in a furnace at 1000 °C for 24 hours in a 95% Ar and 5% H₂ environment and re-measured again as shown in Figure 3(c) where the cut-off absorption peaks remain high, thus demonstrating the high temperature structural robustness of the MDPhC.\[21\] An approximate >8% drop in absorption is observed at higher frequencies above 3 eV due to the surface diffusion of the structure. The homologous temperatures of the furnace test for ruthenium, HfO₂, and Al₂O₃ are \(T_{H,Ru} = 0.49\), \(T_{H,HfO_2} = 0.42\), and \(T_{H,Al_2O_3} = 0.54\), respectively, where diffusion effects are typically expected to be observed. SEM images of the ARC covered areas before and after the furnace test shown in Figure 3(d) and (e), respectively, show no physical damage on the top surface. However, SEM images of areas with no ARC layer before and after the furnace test shown in Figure 3(f) and (g), respectively, show extensive surface diffusion and detachment of the ruthenium from the HfO₂.

A FIB cross section image of a post-furnace ARC area is shown in Figure 3(h), where detachment and surface diffusion of the Ru are still observed underneath the ARC coating. We suspect that the poor adhesion between the Ru and HfO₂ caused the delamination between the two materials during the heating and cooling of the chip. The delamination then allowed for substantial surface diffusion of Ru. The top ARC coating does prevent the Ru from diffusing up and out of the plane of the MDPhC, as seen in Figure 3(g), thus reducing one of the diffusion paths and increasing the survivability of the cavities. If the delamination between the metal and dielectric layers can be prevented via improved adhesion between the layers, then surface diffusion of the metal structures with small radii of curvatures may be suppressed.\[21\] Further study of possible adhesion layers, such as TiN, is underway to prevent delamination at higher temperatures and to test the suppressed surface diffusion.\[34\] Despite the surface diffusion of Ru, the HfO₂, and Al₂O₃ act as a mold to retain the shape of the metallic cavities during the diffusion process. As a result, the cavity modes remain in the post-furnace absorption spectrum, showing the robustness of the cavity modes to altered geometries due to high temperature effects. ARC samples were also placed under solar concentrated (259.11×±11.23 at 25.9 W/cm²) light for 1 minute on/off pulses for up to 10 iterations reaching temperatures up to 900 °C measured via a bonded thermocouple and showed no sign of physical degradation.

In conclusion, we experimentally demonstrate a solar broadband, wide angle, high temperature stable, and wafer-scale fabricated solar absorber. The MDPhC presented here is well suited for solar absorbing applications involving high levels of diffuse, optical concentration, and high temperatures. We demonstrate that a fully encapsulated metal in a dielectric is beneficial for high temperature robustness. Furthermore, absorption of the entire solar spectrum on a single layer metal surface in the MDPhC, allows for ultra-thin absorbers, further extending applications into flexible absorbers/emitters, photoelectrolysis, and hot-electron generation.\[31,32\] The wafer-scale fabricated compatibility of the MDPhC will lead to low-cost and mass producible next-generation solar energy converting devices. The MDPhC structure may be designed with various alternative metals and dielectrics to suit any application’s needs. Although the selection of ALD depositable metals is limited, we experimentally confirmed that sputtered deposition of tungsten had similar conformal coverage, thus drastically expanding the selection of metals (see Supporting Information). With further optimization of the structure and materials, MDPhCs could play a critical role in the future of solar energy conversion.

**Experimental Section**

**Absorption Measurements:** The absolute reflection was measured with a commercial diffuse reference (Labsphere diffuse reflectance standard) with its own known reflection spectrum. An FTIR was used to measure the specular reflection from the wavelength range 1µm to 4 µm. A commercial reference aluminum coated mirror (Thorlabs) was used as the reference with its own known reflection spectrum at angles 30°, 45°, 50°, 60°, and 70°. In both reflection measurements the optical source was an unpolarized broadband source.\[35\]

**FDTD Simulations:** A commercial-grade simulator based on the finite-difference time-domain method was used to perform the calculations.\[35\] A Drude-Lorentz model of the metal was obtained by fitting room temperature measured reflection spectra of ALD deposited ruthenium as shown in Figure 2(a). The dielectric HfO₂ was modeled with a complex permittivity modeled based on measured ALD deposited HfO₂, with a long wavelength index of \(n = 2.04\). Absorption in the HfO₂ was experimentally measured to be zero for photon energies 4.96 eV and below. The optical source is a Gaussian distributed broadband pulse. The absorption spectra were simulated with an \(E_{polarized} \) plane wave at normal incidence. The Al₂O₃ was modeled as a lossless dielectric with index \(n = 1.5\). The simulated total transmission, \(T_v\), through the MDPhC is shown to verify that the MDPhC is in fact absorbing the majority of the input light.

**RCWA Simulations:** The metal is modeled with a complex permittivity, identical to the model used in the FDTD simulation. The HfO₂ is modeled as a lossless dielectric with constant index \(n = 2.04\). The dimensions used are identical to those in the FDTD simulation. A total number of 125 Fourier expansion orders are used for each spectrum.

**Supporting Information**

Supporting Information is available from the Wiley Online Library or from the author.

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